

## Research Paper

# Kinetic Considerations for the Quantitative Assessment of Efflux Activity and Inhibition: Implications for Understanding and Predicting the Effects of Efflux Inhibition

J. Cory Kalvass<sup>1</sup> and Gary M. Pollack<sup>2,3</sup>

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**Purpose.** Unexpected and complex experimental observations related to efflux transport have been reported in the literature. This work was conducted to develop relationships for efflux activity ( $PS_{\text{efflux}}$ ) as a function of commonly studied kinetic parameters [permeability-surface area product (PS), efflux ratio (ER), degree of efflux inhibition ( $\phi_i$ ), 50% inhibitory concentration ( $IC_{50}$ ), and Michaelis-Menten constant ( $K_m$ )].

**Methods.** A three-compartment model (apical, cellular, and basolateral) was used to derive flux equations relating the initial rate of flux and steady-state mass transfer in the presence or absence of active efflux. Various definitions of efflux ratio (ER) were examined in terms of permeability-surface area products. The efflux activity ( $PS_{\text{efflux}}$ ) was expressed in terms of ER and PS. The relationships between  $PS_{\text{efflux}}$  and PS, ER,  $\phi_i$ ,  $IC_{50}$ , and  $K_m$  were solved mathematically. Simulations and examples from the literature were used to illustrate the resulting mathematical relationships.

**Results.** The relationships derived according to a three-compartment model differed fundamentally from commonly accepted approaches for determining  $PS_{\text{efflux}}$ ,  $\phi_i$ ,  $IC_{50}$  and  $K_m$ . Based on the model assumptions and mathematical derivations, currently used mathematical relationships erroneously imply that efflux activity is proportional to change in PS (i.e., flux or  $P_{\text{app}}$ ) and thus underestimate  $PS_{\text{efflux}}$  and  $\phi_i$ , and overestimate  $IC_{50}$  and  $K_m$ .

**Conclusions.** An understanding of the relationship between efflux inhibition and kinetic parameters is critical for appropriate data interpretation, standardization in calculating and expressing the influence of efflux transport, and predicting the clinical significance of efflux inhibition.

**KEY WORDS:** absorption; blood-brain barrier; breast cancer resistance protein (BCRP); Caco-2; efflux inhibition; efflux ratio; efflux transporters; MDCK; multidrug resistance; P-glycoprotein; transcellular flux.

<sup>1</sup>Division of Drug Delivery and Disposition, School of Pharmacy, Kerr Hall C.B.# 7360 University of North Carolina at Chapel Hill, Chapel Hill, North Carolina 27599-7360, USA.

<sup>2</sup>Division of Pharmacotherapy and Experimental Therapeutics, School of Pharmacy, Kerr Hall C.B.# 7360 University of North Carolina at Chapel Hill, Chapel Hill, North Carolina 27599-7360, USA.

<sup>3</sup>To whom correspondence should be addressed. (e-mail: gary\_pollack@unc.edu)

**ABBREVIATIONS:**  $\phi_i$ , degree of efflux inhibition;  $ER_{\alpha}$ , asymmetry efflux ratio ( $PS_{B \rightarrow A}/PS_{A \rightarrow B}$ ) or steady-state ( $C_A/C_B$ );  $ER_A$ , apical efflux ratio ( $PS_{0,B \rightarrow A}/PS_{B \rightarrow A}$ ) or steady-state ( $C_{A,0}/C_A$ );  $ER_B$ , basolateral efflux ratio ( $PS_{I,A \rightarrow B}/PS_{A \rightarrow B}$ ) or steady-state ( $C_{B,I}/C_B$ );  $ER_C$ , cellular efflux ratio ( $PS_{I,A \rightarrow C}/PS_{A \rightarrow C}$ ) or steady-state ( $C_{C,I}/C_C$ );  $[I]$ , inhibitor concentration;  $IC_{50}$ , 50% inhibitory concentration;  $K_i$ , inhibitor constant;  $K_m$ , Michaelis-Menten constant; PS, observed permeability-surface area product;  $PS_0$ , permeability-surface area product in the absence of efflux inhibition;  $PS_I$ , permeability-surface area product when efflux is completely inhibited or saturated; passive permeability-surface area product;  $[S]$ , substrate concentration.

**SUBSCRIPTS:** A, apical; B, basolateral; C, cellular; app, apparent; max, maximum; I, efflux is completely inhibited or saturated;  $A \rightarrow B$ , apical to basolateral, apical compartment dosed;  $B \rightarrow A$ , basolateral to apical, basolateral compartment dosed;  $A \rightarrow C$ , apical to cellular, apical compartment dosed.

## INTRODUCTION

Xenobiotic efflux transporters such as P-glycoprotein (P-gp) can influence drug disposition, efficacy, and safety. Inhibition of efflux transporters may have beneficial (e.g., increased absorption, enhanced presentation to the target site) or adverse (e.g., unexpected or dangerous drug interactions) effects (1). Specific efflux inhibitors are in development to increase oral bioavailability, to target therapeutics to the central nervous system (CNS), and to reverse multidrug resistance (MDR) in cancer (2–4). In addition, drug-drug interactions at the level of efflux transporters have been identified and represent an area of increasing interest (5–7).

Various *in vitro* and *in vivo* models have been developed to identify substrates and inhibitors of efflux transporters and to predict the effects of efflux inhibition on drug disposition and action. These models include cell monolayers (Caco-2 and transfected MDCKII cells), perfused organs (brain, liver, kidney, and intestine), and intact animals (transporter-deficient animals [e.g., *mdr1a/b* deficient mice]; coadministration of efflux inhibitors *in vivo*) (8–11). The predictive utility of these models depends on accurate determination of efflux activity ( $PS_{\text{efflux}}$ ), substrate affinity ( $K_m$ ), inhibitor potency ( $IC_{50}$ ), and the degree of efflux inhibition ( $\phi_i$ ). Unfortunately, the relationships between  $PS_{\text{efflux}}$  and these other experimental parameters are poorly understood, leading to data misinterpretation and inaccurate *in vitro-in vivo* predictions.

Several experimental strategies comprised of different designs and data analysis methods have been used to study apical efflux. Often, an observation in one experimental system is used to predict behavior in another system. For example, Caco-2 monolayer flux studies are used to make predictions of intestinal drug absorption in humans. Kinetic, molecular, and computational models are proposed to provide a better understanding of experimental observations and to make predictions of system behavior. Various types of models with differing degrees of complexity have been proposed for apical efflux (8–14). Even though the models differ in complexity and details, most share some common elements: distinct apical, basolateral, and cellular compartments, with efflux transport located on the apical membrane. A comprehensive understanding of system behavior for the most basic model structure, one that incorporates the fewest assumptions, is an important first step in critically evaluating the kinetic consequences of efflux transport.

In the present work, a simple kinetic model based on the prototypical efflux transporter P-gp was constructed and used to derive the theoretical relationships between  $PS_{\text{efflux}}$  and experimental parameters ( $K_m$ ,  $IC_{50}$ , and  $\phi_i$ ). The resulting mathematical relationships were compared to commonly accepted approaches for calculating  $PS_{\text{efflux}}$ ,  $\phi_i$ ,  $K_m$ , and  $IC_{50}$ . Kinetic considerations suggest that commonly used relationships for determining the experimental parameters  $PS_{\text{efflux}}$ ,  $K_m$ , and  $IC_{50}$  may be confounded by the efflux activity of the model system as well as the choice of substrate.

## THEORETICAL

The simplest kinetic model consistent with efflux attenuating initial rate of apical-to-basolateral (A-to-B) flux is a

three-compartment system (Fig. 1) in which  $PS_A$  and  $PS_B$  represent the passive permeability-surface area product of the apical and basolateral membrane, respectively, and  $PS_{\text{efflux}}$  represents the permeability-surface area product due to efflux transport. This scheme has been used to represent apical efflux (8,14) and is capable of representing the *in vitro* and *in vivo* models used to study the impact of efflux transporters (Table I). The kinetic model associated with this scheme can be described by the following set of differential equations:

$$\frac{dX_A}{dt} = C_C(PS_A + PS_{\text{efflux}}) - C_A PS_A \quad (1-1)$$

$$\frac{dX_C}{dt} = C_A PS_A + C_B PS_B - C_C(PS_A + PS_B + PS_{\text{efflux}}) \quad (1-2)$$

$$\frac{dX_B}{dt} = C_C PS_B - C_B PS_B \quad (1-3)$$

where  $dX_A/dt$ ,  $dX_B/dt$  and  $dX_C/dt$  represent the substrate flux into and out of the apical, basolateral, and cellular compartments, respectively;  $C_A$ ,  $C_B$ , and  $C_C$  represent substrate concentration in each compartment;  $PS_A$  and  $PS_B$  represent the passive permeability-surface area product of the apical and basolateral membranes; and  $PS_{\text{efflux}}$  represents the permeability-surface area product of efflux activity. When substrate concentrations approach or exceed the  $K_m$  for the efflux transport protein:

$$PS_{\text{efflux}} = \frac{PS_{\text{efflux,max}}}{C_C + K_m} \quad (1-4)$$

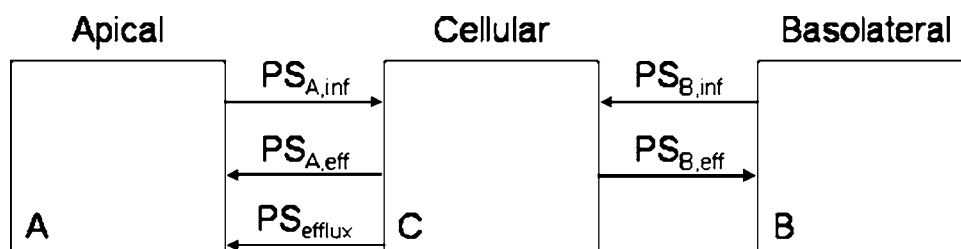
where  $PS_{\text{efflux,max}}$  equals maximal efflux activity.

### Initial Rate of B-to-A Flux in the Presence or Absence of Active Efflux

Assuming initial unidirectional flux into the apical compartment (i.e.,  $X_A=0$ ) and rapid equilibration between the basolateral and cellular compartments ( $dX_C/dt=0$ ), the flux in the B-to-A direction and the concentration in the cellular compartment ( $C_C$ ) can be described by Eqs. (2-1) and (2-2), respectively.

$$\frac{dX_A}{dt} = C_C(PS_A + PS_{\text{efflux}}) \quad (2-1)$$

$$C_C = \frac{C_B PS_B}{(PS_A + PS_B + PS_{\text{efflux}})} \quad (2-2)$$



**Fig. 1.** Three-compartment model consistent with efflux attenuating the initial rate of flux in the A-to-B direction.  $PS_{A,inf}$  and  $PS_{A,eff}$  represent the passive permeability-surface area product of the apical membrane, whereas,  $PS_{B,inf}$  and  $PS_{B,eff}$  represent the passive permeability-surface area products of the basolateral membrane.  $PS_{\text{efflux}}$  represents the permeability-surface area product of efflux activity. It is assumed  $PS_{A,inf} = PS_{A,eff} = PS_A$  and  $PS_{B,inf} = PS_{B,eff} = PS_B$ .

Substitution of Eq. (2-2) into Eq. (2-1) yields the B-to-A flux equation:

$$\frac{dX_{A,B \rightarrow A}}{dt} = \frac{C_B \times PS_B \times (PS_A + PS_{\text{efflux}})}{PS_A + PS_B + PS_{\text{efflux}}} \quad (2-3)$$

In the absence of efflux ( $PS_{\text{efflux}} = 0$ ), the flux in the B-to-A direction is given by:

$$\frac{dX_{A,B \rightarrow A}^{\text{w/o efflux}}}{dt} = \frac{C_B \times PS_B \times PS_A}{PS_A + PS_B} \quad (2-4)$$

**Initial Rate of A-to-B Flux in the Presence or Absence of Active Efflux**

Assuming initial unidirectional flux into the basolateral compartment (i.e.,  $X_B = 0$ ) and rapid equilibration between the apical and cellular compartments ( $dX_C/dt = 0$ ), the flux in the A-to-B direction and the concentration in the cellular compartment ( $C_C$ ) can be described by Eqs. (3-1) and (3-2), respectively:

$$\frac{dX_B}{dt} = C_C PS_B \quad (3-1)$$

$$C_C = \frac{C_A PS_A}{(PS_A + PS_B + PS_{\text{efflux}})} \quad (3-2)$$

Substitution of Eq. (3-2) into Eq. (3-1) yields the A-to-B flux equation:

$$\frac{dX_{B,A \rightarrow B}}{dt} = \frac{C_A \times PS_A \times PS_B}{PS_A + PS_B + PS_{\text{efflux}}} \quad (3-3)$$

In the absence of efflux ( $PS_{\text{efflux}} = 0$ ), A-to-B flux is given by Eq. (3-4):

$$\frac{dX_{B,A \rightarrow B}^{\text{w/o efflux}}}{dt} = \frac{C_A \times PS_A \times PS_B}{PS_A + PS_B} \quad (3-4)$$

**Initial Rate of Cellular Influx**

Assuming initial unidirectional uptake into the cellular compartment (i.e.,  $X_C = 0$ ), flux into the cellular compartment ( $C_C$ ) can be described by Eqs. (4-1) and (4-2) following administration into the apical and basolateral compartments, respectively:

$$\frac{dX_C}{dt} = C_A PS_A \quad (4-1)$$

$$\frac{dX_C}{dt} = C_B PS_B \quad (4-2)$$

**Table I.** Apical, Cellular, and Basolateral Compartments of Various Model Systems

Model system	Apical	Cellular	Basolateral	Relevant ER <sup>a</sup>
Cell monolayer	Apical chamber	Cell monolayer	Basolateral chamber	ER <sub>A</sub> —absorption ER <sub>B</sub> —secretion ER <sub>α</sub> —intracellular concentration
Calcein-AM assay	Extracellular space	Intracellular space	N/A	ER <sub>A</sub> —not applicable ER <sub>B</sub> —not applicable ER <sub>α</sub> —intracellular concentration
MDR cell	Extracellular space	Intracellular space	N/A	ER <sub>A</sub> —not applicable ER <sub>B</sub> —not applicable ER <sub>α</sub> —intracellular concentration
MDR cell	Extracellular space	Cellular membrane	Intracellular space	ER <sub>A</sub> —efflux from intracellular space ER <sub>B</sub> —uptake into intracellular space ER <sub>α</sub> —membrane concentration
Intestine	GI lumen	Epithelial cell	Blood	ER <sub>A</sub> —intestinal absorption ER <sub>B</sub> —intestinal secretion ER <sub>α</sub> —intracellular concentration
Kidney	Tubule lumen (urine)	Tubule epithelial cell	Blood	ER <sub>A</sub> —not applicable ER <sub>B</sub> —renal secretion ER <sub>α</sub> —intracellular concentration
Liver	Canalicular space (bile)	Hepatocyte	Blood	ER <sub>A</sub> —not applicable ER <sub>B</sub> —secretion from blood to bile ER <sub>α</sub> —hepatocyte intracellular concentration
Blood-brain barrier	Capillary lumen (blood)	Endothelial cell	Brain	ER <sub>A</sub> —brain uptake ER <sub>B</sub> —brain efflux ER <sub>α</sub> —brain-to-plasma ratio

<sup>a</sup> Relevant efflux ratio for each experimental system.

### Steady-State Concentrations in Compartments A, B, and C

The steady-state substrate concentration in compartments A, B, and C can be determined by solving differential Eqs. (1-1), (1-2), and (1-3) for concentration at infinite time after administration of mass  $X_0$  to the system:

$$C_{A(t=\infty)} = \frac{X_{A(t=\infty)}}{V_A} \quad (5-1)$$

$$= \frac{X_0(PS_A + PS_{\text{efflux}})}{(PS_{\text{efflux}} \times V_A) + PS_A(V_A + V_B + V_C)}$$

$$C_{B(t=\infty)} = \frac{X_{B(t=\infty)}}{V_B} \quad (5-2)$$

$$= \frac{X_0 \times PS_A}{(PS_{\text{efflux}} \times V_A) + PS_A(V_A + V_B + V_C)}$$

$$C_{C(t=\infty)} = \frac{X_{C(t=\infty)}}{V_C} \quad (5-3)$$

$$= \frac{X_0 \times PS_A}{(PS_{\text{efflux}} \times V_A) + PS_A(V_A + V_B + V_C)}$$

In the absence of active efflux, the steady-state concentrations in compartments A, B, and C are equivalent, and may be expressed as:

$$C_{(t=\infty)}^{w/o \text{ efflux}} = \frac{X_0}{(V_A + V_B + V_C)} \quad (5-4)$$

### Definition of Basolateral Efflux Ratio and Efflux Activity

The basolateral efflux ratio ( $ER_B$ ) can be defined as the ratio of the initial rate of flux in the A-to-B direction when efflux is inhibited completely [Eq. (3-4)] divided by the initial rate of flux in the A-to-B direction when efflux is not inhibited [Eq. (3-3)]:

$$ER_B = \frac{\frac{dX_{B,A \rightarrow B}^{w/o \text{ efflux}}}{dt}}{\frac{dX_{B,A \rightarrow B}}{dt}} = \frac{PS_A + PS_B + PS_{\text{efflux}}}{PS_A + PS_B} \quad (6-1)$$

Alternatively,  $ER_B$  can be defined as the steady-state concentration in the basolateral compartment when efflux is inhibited completely [Eq. (5-4)] divided by the steady-state concentration in the basolateral compartment when efflux is not inhibited [Eq. (5-2)]:

$$ER_{B(t \rightarrow \infty)} = \frac{C_B^{w/o \text{ efflux}}}{C_B} = 1 + \frac{PS_{\text{efflux}} \times V_A}{PS_A(V_A + V_B + V_C)} \quad (6-2)$$

Efflux activity ( $PS_{\text{efflux}}$ ) can be expressed in terms of  $ER_B$  by rearrangement of Eqs. (6-1) and (6-2):

$$PS_{\text{efflux}} = (PS_A + PS_B)(ER_B - 1) \quad (6-3)$$

$$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)}{V_A} PS_A (ER_{B(t \rightarrow \infty)} - 1) \quad (6-4)$$

### Definition of Asymmetry Efflux Ratio and Efflux Activity

Assuming that donor concentrations are identical ( $C_A = C_B$ ), the asymmetry efflux ratio ( $ER_\alpha$ ) can be defined as the ratio of the initial rate of flux in the B-to-A direction [Eq. (2-3)] divided by the initial rate of flux in the A-to-B direction [Eq. (3-3)]:

$$ER_\alpha = \frac{\frac{dX_{A,B \rightarrow A}}{dt}}{\frac{dX_{B,A \rightarrow B}}{dt}} = \frac{PS_A + PS_{\text{efflux}}}{PS_A} \quad (7-1)$$

Alternatively,  $ER_\alpha$  can be defined as the apical steady-state concentration [Eq. (5-1)] divided by the steady-state concentration in the basolateral compartment [Eq. (5-2)]:

$$ER_{\alpha(t \rightarrow \infty)} = \frac{C_A}{C_B} = \frac{PS_A + PS_{\text{efflux}}}{PS_A} \quad (7-2)$$

Efflux activity ( $PS_{\text{efflux}}$ ) then can be solved in terms of  $ER_\alpha$  as:

$$PS_{\text{efflux}} = PS_A(ER_\alpha - 1) \quad (7-3)$$

$$PS_{\text{efflux}} = PS_A(ER_{\alpha(t \rightarrow \infty)} - 1) \quad (7-4)$$

### Definition of Cellular Efflux Ratio and Efflux Activity

The cellular efflux ratio ( $ER_C$ ) can be defined as the ratio of the initial rate of flux in the A-to-C direction when efflux is inhibited completely [Eq. (4-1)] divided by the initial rate of flux in the A-to-C direction when efflux is not inhibited [Eq. (4-1)]:

$$ER_C = \frac{\frac{dX_{C,A \rightarrow C}^{w/o \text{ efflux}}}{dt}}{\frac{dX_{C,A \rightarrow C}}{dt}} = 1 \quad (8-1)$$

$ER_C$  also can be defined as the steady-state concentration in the cellular compartment when efflux is inhibited completely [Eq. (5-4)] divided by the steady-state concentration in the cellular compartment when efflux is not inhibited [Eq. (5-3)]:

$$ER_{C(t \rightarrow \infty)} = \frac{C_C^{w/o \text{ efflux}}}{C_C} = 1 + \frac{PS_{\text{efflux}} \times V_A}{PS_A(V_A + V_B + V_C)} \quad (8-2)$$

Efflux activity ( $PS_{\text{efflux}}$ ) can be expressed in terms of  $ER_C$  as:

$$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)}{V_A} PS_A (ER_{C(t \rightarrow \infty)} - 1) \quad (8-3)$$

### Definition of Apical Efflux Ratio and Efflux Activity

The apical efflux ratio ( $ER_A$ ) can be defined as the ratio of the initial rate of flux in the B-to-A direction when efflux

is not inhibited [Eq. (2–3)] divided by the initial rate of flux in the B-to-A direction when efflux is inhibited completely [Eq. (2–4)]:

$$\begin{aligned} ER_A &= \frac{\frac{dX_{A,B \rightarrow A}}{dt}}{\frac{dX_{A,B \rightarrow A}^{w/o \text{ efflux}}}{dt}} = \frac{(PS_A + PS_B)(PS_A + PS_{\text{efflux}})}{PS_A(PS_A + PS_B + PS_{\text{efflux}})} \\ &\leq \frac{(PS_A + PS_B)}{PS_A} \end{aligned} \quad (9-1)$$

Alternatively,  $ER_A$  can be defined as the steady-state concentration in the apical compartment when efflux is not inhibited [Eq. (5–1)] divided by the observed steady-state concentration in the apical compartment when efflux is inhibited completely [Eq. (5–4)]:

$$\begin{aligned} ER_{A(t \rightarrow \infty)} &= \frac{C_A}{C_A^{w/o \text{ efflux}}} \\ &= \frac{(PS_A + PS_{\text{efflux}})(V_A + V_B + V_C)}{(PS_{\text{efflux}} \times V_A) + PS_A(V_A + V_B + V_C)} \\ &\leq \frac{V_A + V_B + V_C}{V_A} \end{aligned} \quad (9-2)$$

Efflux activity ( $PS_{\text{efflux}}$ ) then can be expressed in terms of  $ER_A$  as:

$$PS_{\text{efflux}} = \frac{(PS_A + PS_B)PS_A(ER_A - 1)}{(PS_A + PS_B) - (PS_A \times ER_A)} \quad (9-3)$$

$$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)PS_A(ER_A - 1)}{(V_A + V_B + V_C) - (V_A \times ER_A)} \quad (9-4)$$

## RESULTS AND DISCUSSION

### Efflux Activity is Proportional to the Quantity ER-1, not to Attenuation or Enhancement of Flux

The mathematical relationships derived from the three-compartment model in Fig. 1 indicate that efflux attenuates flux in the A-to-B direction and enhances flux in the B-to-A direction. However, neither the attenuation of flux in the A-to-B nor the enhancement of flux in the B-to-A direction is proportional to the efflux activity ( $PS_{\text{efflux}}$ ) [Eqs. (2–3) and (3–3); illustrated in Fig. 2]. In contrast, according to the three-compartment model [Table II; illustrated in Fig. 3; and Eqs. (6–3), (6–4), (7–3), (7–4), and (8–3)],  $PS_{\text{efflux}}$  is proportional to  $ER_{B-1}$ ,  $ER_{\alpha-1}$ , and  $ER_{C-1}$ . The fact that  $PS_{\text{efflux}}$  is not proportional to flux but is proportional to  $ER_{B-1}$ ,  $ER_{\alpha-1}$ , and  $ER_{C-1}$  has important implications regarding the calculation of  $PS_{\text{efflux}}$ ,  $K_m$ , and  $IC_{50}$ .

Numerous approaches with little consensus have been proposed to calculate and express  $PS_{\text{efflux}}$  (Table III). Often,  $PS_{\text{efflux}}$  is calculated directly from the magnitude of attenuation or enhancement in flux caused by efflux. Since the magnitude of attenuation and enhancement in flux is not proportional to  $PS_{\text{efflux}}$ , and therefore should not be used to calculate  $PS_{\text{efflux}}$  directly, we propose a novel method,

consistent with the simple three-compartment model for calculating and expressing  $PS_{\text{efflux}}$ .

From previous mathematical derivations,  $PS_{\text{efflux}}$  can be defined in terms of  $PS_A$ ,  $PS_B$ , and efflux ratios (Table II), and is proportional to  $ER_{\alpha-1}$ ,  $ER_{B-1}$ , and  $ER_{C(t \rightarrow \infty)-1}$  (Table II; illustrated in Fig. 3). However, in most experimental designs,  $PS_A$  and  $PS_B$  are not determined, but the passive permeability-surface area product in the A-to-B direction ( $PS_{I,A \rightarrow B}$ ) is measured. The  $PS_{I,A \rightarrow B}$  can be expressed in terms of  $PS_A$  and  $PS_B$  as follows:

$$PS_{I,A \rightarrow B} = \frac{PS_A \times PS_B}{PS_A + PS_B} \quad (10-1)$$

If  $PS_A$  and  $PS_B$  are assumed to be equal, rearrangement of Eq. (10–1) indicates that  $PS_A$  and  $PS_B$  equal  $2PS_{I,A \rightarrow B}$ .  $PS_{\text{efflux}}$  can be expressed in terms of  $PS_{I,A \rightarrow B}$  and ER by substituting  $2PS_{I,A \rightarrow B}$  for  $PS_A$  and  $PS_B$  into Eqs. (6–3), (7–3), and (8–3), yielding Eqs. (10–2), (10–3), and (10–4) respectively:

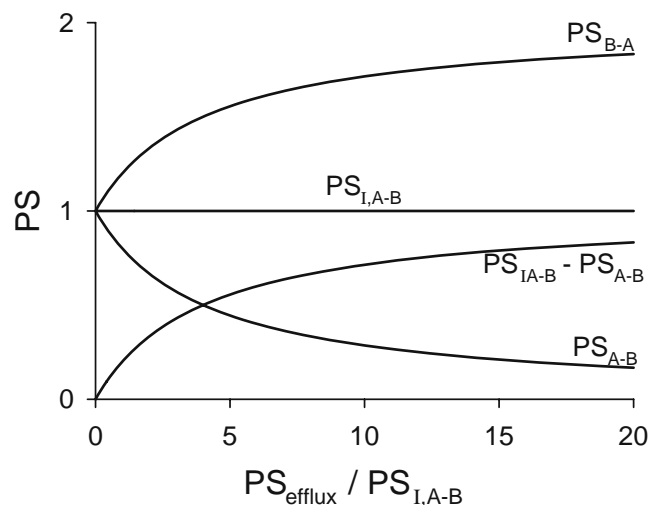
$$PS_{\text{efflux}} = 4PS_{I,A \rightarrow B}(ER_B - 1) \quad (10-2)$$

$$PS_{\text{efflux}} = 2PS_{I,A \rightarrow B}(ER_{\alpha} - 1) \quad (10-3)$$

$$PS_{\text{efflux}} = 2PS_{I,A \rightarrow B} \frac{(V_A + V_B + V_C)}{V_A} (ER_{C(t \rightarrow \infty)} - 1) \quad (10-4)$$

From the preceding equations, the precise value of  $PS_{\text{efflux}}$  can be expressed in terms of commonly obtained experimental parameters, namely efflux ratio and passive permeability. In qualitative terms,  $PS_{\text{efflux}}$  is proportional to ER-1 multiplied by the passive permeability. This relationship differs from other commonly cited approaches for expressing  $PS_{\text{efflux}}$ ; however, it is kinetically sound (based on the inherent assumptions of the model in Fig. 1), and it is intuitive in that the efflux ratio of a substrate is dependent on both efflux activity and the substrate passive permeability. Expressing  $PS_{\text{efflux}}$  in terms of  $PS_{I,A \rightarrow B}$  and ER also is convenient, and allows for precise quantitation and comparison of  $PS_{\text{efflux}}$  between different substrates, model systems, and laboratories.

As in the case for  $PS_{\text{efflux}}$ , flux should not be used to directly calculate  $K_m$  or  $IC_{50}$ . This is true because, when determining  $K_m$  or  $IC_{50}$ , it is necessary to relate substrate or inhibitor concentrations to the value  $PS_{\text{efflux}}$  and because flux is not proportional to  $PS_{\text{efflux}}$ . Instead of using flux,  $K_m$  and  $IC_{50}$  may be calculated directly from  $ER_{\alpha-1}$ ,  $ER_{B-1}$ , and  $ER_{C(t \rightarrow \infty)-1}$  since ER-1 is proportional to  $PS_{\text{efflux}}$ . The difference between calculating  $IC_{50}$  directly from  $P_{\text{app}}$  versus ER-1 can be illustrated with a recent example from the literature. Although numerous relevant data sets can be found in the literature, a data set from Chen *et al.* (2002) was chosen due to the high quality of the data and the extensive characterization of the Michaelis–Menten profile (Fig. 4) (15). The conclusions drawn from consideration of this experimental data set are generalizable to other situations. Briefly, the investigators used an *in situ* rat brain perfusion technique to examine the ability of the P-gp inhibitor GF-120918 to inhibit the P-gp-mediated efflux of quinidine.



**Fig. 2.** Relationship between efflux activity ( $PS_{\text{efflux}}$ ) and permeability-surface area product (PS). Efflux activity was normalized for the A-to-B passive permeability-surface area product ( $PS_{I,A-B}$ ).  $PS_A$  and  $PS_B$  were assumed to be equal, therefore  $PS_{I,A-B} = 1/2 PS_A$ . Since  $P_{\text{app}}$  and flux are proportional to PS, substituting  $P_{\text{app}}$  or flux for PS will yield the identical relationship.

Various concentrations of GF-120918 were examined; as concentrations of GF-120918 were increased, the  $P_{\text{app}}$  value for quinidine increased to a plateau at  $\sim 13$ -fold. In such experiments, the  $IC_{50,\text{app}}$  of the inhibitor often is calculated by fitting a modified Michaelis-Menten equation to the  $P_{\text{app}}$  vs. inhibitor concentration data. In order to illustrate why  $IC_{50,\text{app}}$  should not be calculated in this manner, we used a modified Michaelis-Menten equation to calculate both the  $IC_{50,\text{app}}$  (from the  $P_{\text{app}}$  and GF-120918 concentration data) and the “true”  $IC_{50}$  (from ER and GF-120918 data). Even though the same experimental data were used in calculating  $IC_{50,\text{app}}$  and  $IC_{50}$ , the  $IC_{50,\text{app}}$  ( $0.56 \mu\text{M}$ ) was 13-fold higher than the  $IC_{50}$  ( $0.042 \mu\text{M}$ ). It is clear that the  $IC_{50,\text{app}}$

calculated from  $P_{\text{app}}$  data differs fundamentally from the  $IC_{50}$  calculated from ER data. Since changes in  $P_{\text{app}}$  are not proportional to changes in  $PS_{\text{efflux}}$ ,  $IC_{50}$  and  $K_m$  should not be calculated by fitting a modified Michaelis-Menten equation to  $P_{\text{app}}$  data. Mathematical treatment of  $IC_{50}$  and  $K_m$  will be explored in further detail in a later section; at this point, we simply demonstrate that calculating  $IC_{50}$  or  $K_m$  from flux or  $P_{\text{app}}$  values is not equivalent to calculations based on ER values.

### B-to-A Flux (Secretory Flux) Is Minimally Sensitive to Efflux Activity

Apical efflux clearly enhances flux in the B-to-A direction. However, this enhancement is not proportional to either efflux activity ( $PS_{\text{efflux}}$ ) or  $ER_A^{-1}$  [Eqs. (2–3) and (9–1); illustrated in Figs. 2 and 3]. The fold increase in the B-to-A flux is given by the  $ER_A$  in Eq. (9–1):

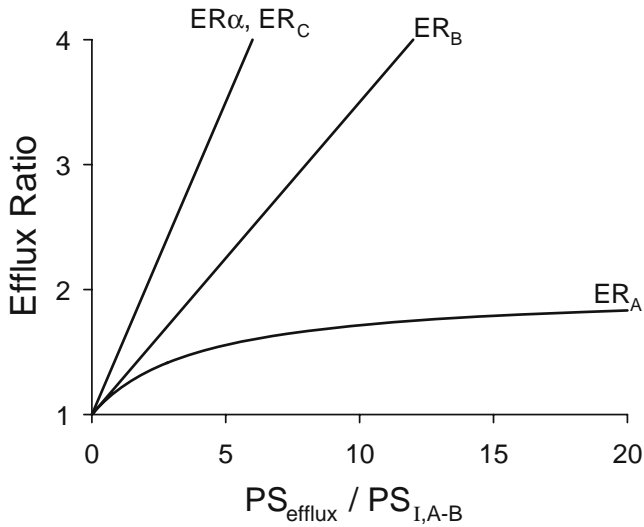
$$ER_A = \frac{\frac{dX_{A,B \rightarrow A}}{dt}}{\frac{dX_{A,B \rightarrow A}^{w/o \text{ efflux}}}{dt}} = \frac{(PS_A + PS_B)(PS_A + PS_{\text{efflux}})}{PS_A(PS_A + PS_B + PS_{\text{efflux}})} \leq \frac{(PS_A + PS_B)}{PS_A} \quad (9-1)$$

Taking into account the model assumptions discussed previously, the maximum value of  $ER_A$  is  $(PS_A + PS_B)/PS_A$  (i.e., 2, assuming  $PS_A = PS_B$ ). In other words, if passive permeabilities across the apical and basolateral membranes are similar, then the maximum increase in B-to-A flux that efflux can cause is twofold. Therefore, measuring the effect of efflux on permeability in the B-to-A direction is uninformative, as flux in the B-to-A direction is not proportional to, and is in fact minimally sensitive to,  $PS_{\text{efflux}}$ .

Experimental evidence is consistent with this predicted behavior. For example, the B-to-A flux of loperamide, amprenavir, and eletriptan in MDR1-transfected MDCK cell monolayers increased only 1.5- to 2.1-fold despite a 10-, 29-,

**Table II.** Relationships Between Efflux Ratio, Permeability-Surface Area Products, and Efflux Activity

Definition of efflux ratio	Assumptions	Efflux activity
$ER_B = \frac{\frac{dX_{B,A \rightarrow B}^{w/o \text{ efflux}}}{dt}}{\frac{dX_{B,A \rightarrow B}}{dt}} = \frac{PS_A + PS_B + PS_{\text{efflux}}}{PS_A + PS_B}$	Initial uptake rate (i.e., $X_B=0$ ); rapid equilibrium between A and C	$PS_{\text{efflux}} = (PS_A + PS_B)(ER_B - 1)$
$ER_{B(t \rightarrow \infty)} = \frac{C_B^{w/o \text{ efflux}}}{C_B} = 1 + \frac{PS_{\text{efflux}} \times V_A}{PS_A(V_A + V_B + V_C)}$	None	$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)}{V_A} PS_A (ER_B - 1)$
$ER_\alpha = \frac{\frac{dX_{A,B \rightarrow A}}{dt}}{\frac{dX_{B,A \rightarrow B}}{dt}} = \frac{PS_A + PS_{\text{efflux}}}{PS_A}$	Initial uptake rate (i.e., $X_A=0$ ); rapid equilibrium between B and C initial uptake rate (i.e., $X_B=0$ ); rapid equilibrium between A and C	$PS_{\text{efflux}} = PS_A (ER_\alpha - 1)$
$ER_{\alpha(t \rightarrow \infty)} = \frac{C_A}{C_B} = \frac{PS_A + PS_{\text{efflux}}}{PS_A}$	None	$PS_{\text{efflux}} = PS_A (ER_\alpha - 1)$
$ER_C = \frac{\frac{dX_{C,A \rightarrow C}^{w/o \text{ efflux}}}{dt}}{\frac{dX_{C,A \rightarrow C}}{dt}} = 1$	Initial uptake rate (i.e., $X_C=0$ );	n/a
$ER_{C(t \rightarrow \infty)} = \frac{C_C^{w/o \text{ efflux}}}{C_C} = 1 + \frac{PS_{\text{efflux}} \times V_A}{PS_A(V_A + V_B + V_C)}$	None	$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)}{V_A} PS_A (ER_C - 1)$
$ER_A = \frac{\frac{dX_{A,B \rightarrow A}}{dt}}{\frac{dX_{A,B \rightarrow A}^{w/o \text{ efflux}}}{dt}} = \frac{(PS_A + PS_B)(PS_A + PS_{\text{efflux}})}{PS_A(PS_A + PS_B + PS_{\text{efflux}})} \leq \frac{(PS_A + PS_B)}{PS_A}$	Initial uptake rate (i.e., $X_A=0$ ); rapid equilibrium between B and C	$PS_{\text{efflux}} = \frac{(PS_A + PS_B)PS_A (ER_A - 1)}{(PS_A + PS_B) - (PS_A \times ER_A)}$
$ER_{A(t \rightarrow \infty)} = \frac{C_A}{C_A^{w/o \text{ efflux}}} = \frac{(PS_A + PS_{\text{efflux}})(V_A + V_B + V_C)}{(PS_{\text{efflux}} \times V_A) + PS_A(V_A + V_B + V_C)} \leq \frac{V_A + V_B + V_C}{V_A}$	None	$PS_{\text{efflux}} = \frac{(V_A + V_B + V_C)PS_A (ER_A - 1)}{(V_A + V_B + V_C) - (V_A \times ER_A)}$



**Fig. 3.** Relationship between efflux activity ( $PS_{\text{efflux}}$ ) and asymmetry ( $ER_{\alpha}$ ), absorptive ( $ER_B$ ), secretory ( $ER_A$ ), or intracellular ( $ER_C$ ) efflux ratio. Efflux activity was normalized for the A-to-B passive permeability surface area product ( $PS_{I,A-B}$ ).  $PS_A$  and  $PS_B$  were assumed to be equal, therefore  $PS_{I,A-B} = 1/2 PS_A$ .

and 45-fold decrease in A-to-B flux, respectively (16). Another experimental observation consistent with a maximum twofold increase in B-to-A flux is the influence of P-gp-mediated efflux on the equilibration half-life of fentanyl, alfentanil, methadone, loperamide across the blood-brain barrier (BBB). These opioids were used as *in vivo* probes in P-gp-competent and P-gp-deficient mice to assess the influence of P-gp-mediated efflux on brain-to-plasma ratio ( $K_{p,\text{brain}}$ ) and the pseudo-first-order rate constant governing

the time-dependent approach of the brain-to-plasma ratio to its equilibrium value ( $K_{\text{eq,brain}}$ ). Based on the principle that  $K_{\text{eq,brain}}$  is influenced only by the rate of egress from brain,  $K_{\text{eq,brain}}$  should be directly proportional to  $PS_{B \rightarrow A}$ . Thus, the fold change in  $K_{\text{eq,brain}}$  can be expressed in terms of  $ER_A$ . In contrast, the fold change in brain-to-plasma ratio can be expressed in terms  $ER_{\alpha}$ . So by studying the effect of P-gp-mediated efflux on  $K_{p,\text{brain}}$  and  $K_{\text{eq,brain}}$ , the influence of efflux on the  $ER_{\alpha}$  and  $ER_A$  can be deduced *in vivo*. P-gp-mediated efflux had a more pronounced effect on the brain-to-plasma ratio (1.9- to 44-fold change) than on the brain equilibration half-life (1.0- to 2.4-fold change). Without examining the experimental observations in terms of  $ER_A$  and  $ER_{\alpha}$ , the experimental observations in  $K_{\text{eq,brain}}$  may be difficult to rationalize. However, the results are precisely what would be expected based on the model and associated assumptions (Table IV).

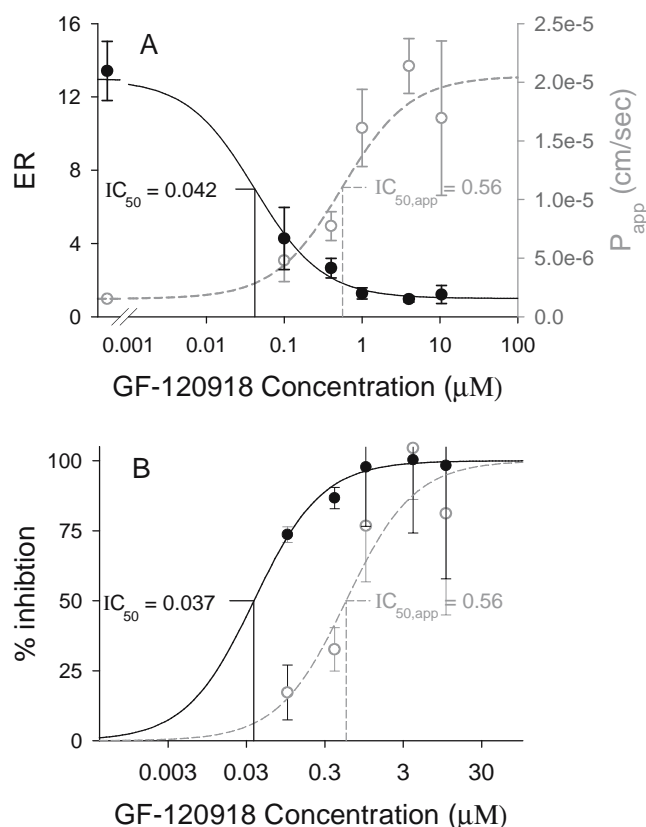
Despite the kinetic considerations, for some substrates apical efflux transport increases flux in the B-to-A direction by more than twofold. For example, in Caco-2 monolayers the efflux transporter P-gp had a pronounced effect (tenfold) on the B-to-A flux of rhodamine 123, even though P-gp efflux minimally attenuated rhodamine 123 flux in the A-to-B direction (17). In the same Caco-2 studies, rhodamine 123 had low membrane permeability, with A-to-B flux occurring primarily by the paracellular route. However, the B-to-A flux was much higher than the A-to-B flux, and it occurred via the transcellular route, because rhodamine 123 was transported across the basolateral membrane by active uptake. Active uptake of rhodamine 123 across the basolateral membrane violates the assumptions of the basic kinetic model ( $PS_{B,\text{inf}} \neq PS_{B,\text{eff}}$ ). Therefore, efflux has a more pronounced effect on B-to-A flux than the kinetic scheme would suggest.

**Table III.** Comparison of Methods for the Calculation of Experimental Parameters

Parameter	Method(s) from literature	Method(s) derived from kinetic theory
$IC_{50}$	$PS = PS_0 + (PS_I - PS_0) \times \frac{[I]}{[I] + IC_{50,\text{app}}}$ (27)	$PS = \frac{PS_I \times PS_0}{PS_I + (PS_0 - PS_I) \times \frac{[I]}{[I] + IC_{50}}}$ $ER - 1 = \left( \frac{PS_I}{PS_0} - 1 \right) \frac{IC_{50}}{[I] + IC_{50}}$
$K_m$	$PS = PS_0 + (PS_I - PS_0) \times \frac{[S]}{[S] + K_{m,\text{app}}}$ (28,29)	$PS = \frac{PS_I \times PS_0}{PS_I + (PS_0 - PS_I) \times \frac{[S]}{[S] + K_m}}$ $ER - 1 = \left( \frac{PS_I}{PS_0} - 1 \right) \frac{K_m}{[S] + K_m}$
$\phi_i$	$\phi_{i,\text{app}} = \frac{PS - PS_0}{PS_I - PS_0}$ (30)	$\phi_i = \frac{ER_{\text{max}} - ER}{ER_{\text{max}} - 1}$ $\phi_i = \frac{PS_I}{PS} \times \frac{(PS - PS_0)}{(PS_I - PS_0)}$
	$\phi_{i,\text{app}} = 1 - \frac{PS_{B \rightarrow A} - PS_{A \rightarrow B}}{PS_{0,B \rightarrow A} - PS_{0,A \rightarrow B}}$ (31)	$\phi_i = \frac{PS_{I,A \rightarrow B}}{PS_{A \rightarrow B}} \times \left( 1 - \frac{PS_{B \rightarrow A} - PS_{A \rightarrow B}}{PS_{0,B \rightarrow A} - PS_{0,A \rightarrow B}} \right)$ $\phi_i \geq 1 - \frac{1}{\text{fold} \Delta PS}$ a
$PS_{\text{efflux}}$	$PS_{\text{efflux,app}} = PS_I - PS$ $PS_{\text{efflux,app}} \propto PS_I - PS$ $PS_{\text{efflux,app}} \propto ER_B$ $PS_{\text{efflux,app}} \propto ER_C$ $PS_{\text{efflux,app}} \propto ER_{\alpha}$	$PS_{\text{efflux}} = 4PS_{I,A \rightarrow B}(ER_B - 1)$ $PS_{\text{efflux}} = 2PS_{I,A \rightarrow B}(ER_{\alpha} - 1)$
$K_{m,\text{app}}$	$K_{m,\text{app}} = K_{m,\text{app}}$	$PS_{\text{efflux}} \propto PS_{I,A \rightarrow B}(ER - 1)$ $K_{m,\text{app}} = K_m \times ER_{\text{max}}$
$IC_{50,\text{app}}$	$IC_{50,\text{app}} = IC_{50,\text{app}}$	$IC_{50,\text{app}} = IC_{50} \times ER_{\text{max}}$

Note: Since flux and  $P_{\text{app}}$  are proportional to  $PS$ , flux and  $P_{\text{app}}$  can be substituted for  $PS$   $ER = ER_B$ ,  $ER_C$ , or  $ER_{\alpha}$ .

a Rearrangement of Eq. (12-10).



**Fig. 4.** Influence of GF-120918 on the brain uptake of quinidine. Data from Chen *et al.* (13). (A) *In situ* brain perfusion  $P_{app}$  and ER values for quinidine were determined in the presence of various concentrations of GF-120918 (solid and open symbols, respectively). Modified Michaelis–Menten equations [ $PS = PS_0 + (PS_1 - PS_0) \times \frac{[I]}{[I] + IC_{50,app}}$ ] or  $ER = ER_{max} + (ER_{max} - 1) \times \frac{[I]}{[I] + IC_{50}}$  were fit to the  $P_{app}$  or ER data to obtain estimates of  $IC_{50,app}$  and  $IC_{50}$  respectively. (B) Inhibition of P-gp-mediated efflux was calculated from the  $P_{app}$  data using either Eq. (12–5), a commonly cited inhibition equation (open symbols), or Eq. (12–4), a newly derived inhibition equation (solid symbols), and the Michaelis–Menten equation was fitted to the inhibition data to obtain estimates of  $IC_{50,app}$  and  $IC_{50}$ , respectively. Note that in both panels (A) and (B),  $IC_{50,app}$  overestimated  $IC_{50}$ , and that  $IC_{50,app} = ER_{max} \times IC_{50}$ .

This phenomenon has been observed for other efflux substrates transported by multiple proteins, such as fexofenadine and digoxin (18,19). In cases in which active transport processes are present in addition to efflux, estimates of kinetic efflux parameters ( $IC_{50}$ ,  $K_m$ , or  $PS_{efflux}$ ) may be confounded by the action of the other transport process(es). Experimental determination of efflux transporter kinetic

parameters is difficult when flux is influenced by multiple systems (i.e., active uptake and efflux), because inhibitors often are nonselective and the  $K_m$ (s) of additional active process(es) may be less than that of the efflux transporter.

#### Asymmetry and Basolateral Efflux Ratios are not Identical

The basolateral and asymmetry efflux ratios ( $ER_B$  and  $ER_\alpha$ ) are used to characterize the influence of efflux on a given model system and to extrapolate observations from one model system to another (i.e., *in vitro* to *in vivo* predictions). Thus, it is important to understand the relationship between  $ER_B$  and  $ER_\alpha$ , which may be best understood by examining the relationship between  $ER_\alpha - 1$  and  $ER_B - 1$  from rearrangement of Eqs. (7–3) and (6–3):

$$ER_\alpha - 1 = \left( \frac{PS_A + PS_{efflux}}{PS_A} \right) - 1 \quad (11-1)$$

$$ER_B - 1 = \left( \frac{PS_A + PS_B + PS_{efflux}}{PS_A + PS_B} \right) - 1 \quad (11-2)$$

If  $PS_A = PS_B$ , then the ratio of  $ER_\alpha - 1$  and  $ER_B - 1$  equals 2 as shown in Eq. (11–3).

$$\frac{ER_\alpha - 1}{ER_B - 1} = \frac{\left( \frac{PS_A + PS_{efflux}}{PS_A} \right) - 1}{\left( \frac{PS_A + PS_B + PS_{efflux}}{PS_A + PS_B} \right) - 1} = 2 \quad (11-3)$$

Equation (11–3) illustrates that  $ER_\alpha$  is larger than  $ER_B$  and that, when  $PS_{efflux}$  is large compared to  $PS_A$ ,  $ER_\alpha$  will equal twice  $ER_B$ .

The fact that  $ER_\alpha > ER_B$  may explain why the *in situ* brain perfusion P-gp efflux ratio underpredicts the *in vivo* brain-to-plasma efflux ratio. Several studies have examined the influence of P-gp on brain uptake of P-gp substrates, and developed relationships for the difference in brain uptake clearance ( $Cl_{up}$ ) and brain-to-plasma ratio ( $K_{p,brain}$ ) between P-gp-deficient and P-gp-competent mice. The *in situ* P-gp efflux ratio (9), which is analogous to  $ER_B$  and is determined by dividing  $Cl_{up}$  in P-gp-deficient mice ( $Cl_{up}^{-/-}$ ) by the brain uptake clearance in P-gp-competent mice ( $Cl_{up}^{+/+}$ ), has been used to predict the *in vivo* P-gp efflux ratio, which is calculated by dividing the  $K_{p,brain}$  in P-gp-deficient mice ( $K_{p,brain}^{-/-}$ ) by the  $K_{p,brain}$  in P-gp-competent mice ( $K_{p,brain}^{+/+}$ ). In most studies, the *in situ* efflux ratio correlated well with the *in vivo* efflux ratio, although the *in situ* efflux ratio consistently

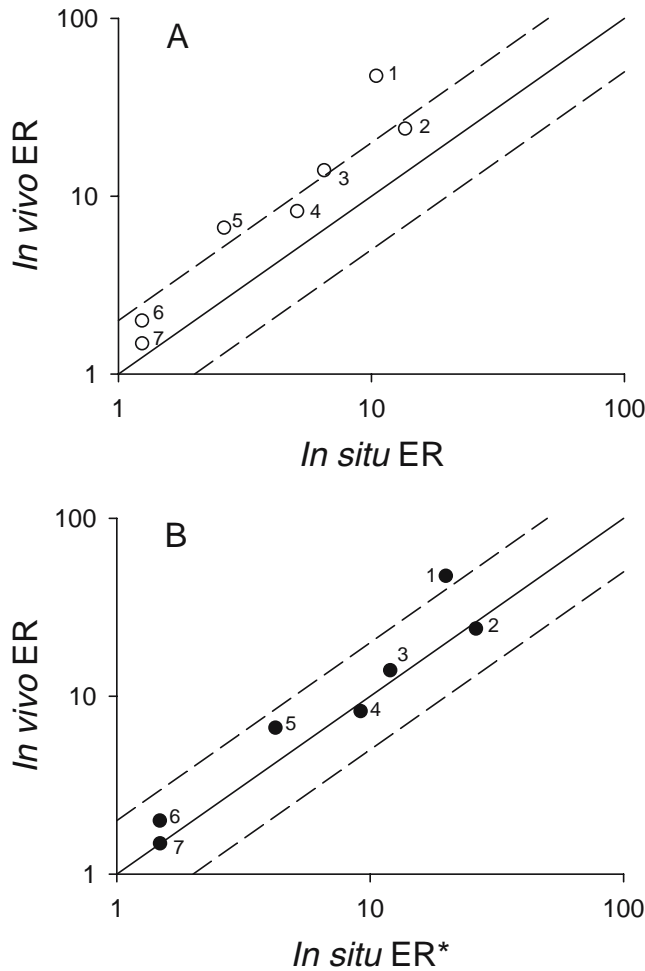
**Table IV.** Influence of P-gp-Efflux on the Brain-to-Plasma Ratio ( $K_{p,brain}$ ) and Brain Equilibration Rate Constant ( $K_{brain,eq}$ ) of P-gp Substrates

	Actual fold change in $K_{p,brain}$ ( $ER_\alpha$ ) <sup>a</sup>	Actual fold change in $K_{brain,eq}$ ( $ER_A$ ) <sup>a</sup>	Expected change in $K_{brain,eq}$ ( $ER_A$ ) <sup>b</sup>
Fentanyl	1.9	1.0	1.3
Alfentanil	2.8	1.4	1.5
Methadone	7.2	2.4	1.8
Loperamide	44	1.9	2

<sup>a</sup> Unpublished experimental observations.

<sup>b</sup> The expected change in change in  $K_{brain,eq}$  was calculated from the fold change in  $K_{p,brain}$  and the theoretical relationship between  $ER_\alpha$  and  $ER_A$ .  $ER_A = 2ER_\alpha / (1 + ER_\alpha)$ .





**Fig. 5.** Correlation between *in situ* and *in vivo* P-gp efflux ratios. (A) *In situ* efflux ratio was by defined as the ratio of brain uptake clearance in P-gp-deficient mice divided by the brain uptake clearance in P-gp-competent mice. *In vivo* efflux ratio was calculated as the brain-to-plasma ratio of P-gp-deficient mice divided by the brain-to-plasma ratio of P-gp-competent animals. In panel (B), *in situ* ER\* was corrected for differences between ER<sub>A</sub> and ER<sub>B</sub> (ER\* = [(ER - 1) × 2] + 1). Solid line represents line of unity whereas dashed lines represent twofold above or below the line of unity. Compound legend is as follows: 1 loperamide, 2 quinidine, 3 ritonavir, 4 verapamil, 5 methadone, 6 fentanyl, 7 morphine.

underpredicted the *in vivo* efflux ratio [Fig. 5; data from references (9,11,20,21) and unpublished observations]. This underprediction is expected since the *in situ* P-gp efflux ratio is analogous to ER<sub>B</sub> and the *in vivo* efflux ratio is analogous to ER<sub>A</sub>. Direct predictions can be made by comparing the *in situ* efflux ratio minus one to the *in vivo* efflux ratio minus one. The *in situ* efflux ratio minus one is expected to equal one half the *in vivo* efflux ratio minus one. When the *in situ* and *in vivo* efflux ratios are compared in this manner, the *in situ* efflux ratio no longer underpredicts the *in vivo* efflux ratio (Fig. 5).

#### Apparent IC<sub>50</sub> and K<sub>m</sub> are Influenced by Efflux Activity

The efflux activity (PS<sub>efflux</sub>) in the presence of efflux inhibition can be expressed as in Eq. (12-1), where PS<sub>efflux,max</sub> is the efflux activity in the absence of inhibition (i.e., when the

efflux ratio equals ER<sub>max</sub>), and φ<sub>i</sub> is the degree of efflux inhibition:

$$PS_{\text{efflux}} = PS_{\text{efflux,max}} \times (1 - \phi_i) \quad (12-1)$$

As derived previously, the efflux activity (PS<sub>efflux</sub>) is proportional to ER<sub>A</sub>-1, ER<sub>B</sub>-1 and ER<sub>C(t→∞)</sub>-1. When ER-1 and ER<sub>max</sub>-1 are substituted for PS<sub>efflux</sub> and PS<sub>efflux,max</sub> respectively, then Eq. (12-1) can be rewritten as follows:

$$ER - 1 = (ER_{\text{max}} - 1) \times (1 - \phi_i) \quad (12-2)$$

Solving Eq. (12-2) for φ<sub>i</sub> yields:

$$\phi_i = \frac{ER_{\text{max}} - ER}{ER_{\text{max}} - 1} \quad (12-3)$$

From this point forward, the symbol PS will represent any experimental variable that is attenuated by efflux in a manner consistent with the model in Fig. 1, such as PS<sub>A→B</sub> (i.e., P<sub>app</sub> or A-to-B flux), cellular partition ratio, or brain-to-plasma ratio. The efflux ratio (ER) can be defined as (PS<sub>I</sub>/PS), where PS<sub>I</sub> is the value of PS when efflux is inhibited completely. When efflux activity is completely inhibited, ER equals unity. In the absence of any efflux inhibition, ER equals ER<sub>max</sub>, defined as (PS<sub>I</sub>/PS<sub>0</sub>), where PS<sub>0</sub> is the value of PS in the absence of efflux inhibition. Equation (12-3) can be expressed in terms of PS by substituting (PS<sub>I</sub>/PS<sub>0</sub>) and (PS<sub>I</sub>/PS) for ER<sub>max</sub> and ER.

$$\phi_i = \frac{PS_I}{PS} \times \frac{(PS - PS_0)}{(PS_I - PS_0)} \quad (12-4)$$

Equation (12-5) represents the standard equation used to calculate φ<sub>i</sub> in the literature and it differs from Eq. (12-4) by a factor of PS<sub>I</sub>/PS:

$$\phi_{i,\text{app}} = \frac{PS - PS_0}{PS_I - PS_0} \quad (12-5)$$

This difference between the kinetically derived Eq. (12-4) and Eq. (12-5) has a profound impact on calculating IC<sub>50</sub>, K<sub>m</sub>, and understanding the relationship between PS and φ<sub>i</sub> (see Table III). Use of Eq. (12-5) does not yield true kinetic parameters for the system, but rather apparent parameters. This can be illustrated by solving Eqs. (12-4) and (12-5) for PS, yielding Eqs. (12-6) and (12-7), respectively:

$$PS = \frac{PS_I \times PS_0}{PS_I + (PS_0 - PS_I) \times \phi_i} \quad (12-6)$$

$$PS = PS_0 + (PS_I - PS_0) \times \phi_{i,\text{app}} \quad (12-7)$$

Examination of Eq. (12-7) reveals that the maximum increase in PS due to inhibition is PS<sub>I</sub>-PS<sub>0</sub>; when φ<sub>i,app</sub> equals 50%, the increase in PS equals one half the maximum possible increase (i.e., the change in PS is directly proportional to φ<sub>i,app</sub>).

The actual fold change in PS due to efflux inhibition may be expressed in terms of efflux ratios or permeability-surface area products:

$$\text{fold } \Delta PS = \frac{PS}{PS_0} = \frac{PS_I/PS_0}{PS_I/PS} = \frac{ER_{\text{max}}}{ER} \quad (12-8)$$

Solving Eq. (12-3) for ER and substituting into Eq. (12-8) yields:

$$\text{fold } \Delta \text{PS} = \frac{\text{ER}_{\text{max}}}{\text{ER}_{\text{max}} - (\text{ER}_{\text{max}} - 1) \times \phi_i} \quad (12-9)$$

Assuming  $\phi_i = \frac{[I]}{[I] + \text{IC}_{50}}$ , the maximum fold change in PS at any inhibitor concentration [I] is determined by the upper limits of Eq. (12-9):

$$\frac{[I]}{\text{IC}_{50}} + 1 \geq \text{fold } \Delta \text{PS} \leq \text{ER}_{\text{max}} \quad (12-10)$$

According to the theoretically derived Eq. (12-10), at 50% inhibition ( $[I] = \text{IC}_{50}$ ) the maximum increase in PS is twofold. This is contrary to the relationship in Eq. (12-7). However, it is analogous to the case in which 50% inhibition of a specific clearance pathway (i.e., CYP3A4) will result in at most a twofold increase in steady-state concentrations (22).

The difference between the theoretically derived Eq. (12-6) and the simple Eq. (12-7) can be illustrated further by comparing estimates of  $\text{IC}_{50}$  and  $K_m$  obtained from the two equations. The nonlinear relationships between PS and  $\text{IC}_{50}$  derived from the kinetic model in Fig. 1 can be expressed as in Eq. (12-11). Similarly, the relationship between PS and  $K_m$  can be expressed as in Eq. (12-12):

$$\text{PS} = \frac{\text{PS}_I \times \text{PS}_0}{\text{PS}_I + (\text{PS}_0 - \text{PS}_I) \times \frac{[I]}{[I] + \text{IC}_{50}}} \quad (12-11)$$

$$\text{PS} = \frac{\text{PS}_I \times \text{PS}_0}{\text{PS}_I + (\text{PS}_0 - \text{PS}_I) \times \frac{[S]}{[S] + K_m}} \quad (12-12)$$

Using the relationship in Eq. (12-7), PS can be expressed in terms of  $\text{IC}_{50, \text{app}}$  or  $K_{m, \text{app}}$  by substituting  $\{[I]/([I] + \text{IC}_{50, \text{app}})\}$  or  $\{[S]/([S] + K_{m, \text{app}})\}$  for  $\phi_{i, \text{app}}$ :

$$\text{PS} = \text{PS}_0 + (\text{PS}_I - \text{PS}_0) \times \frac{[I]}{[I] + \text{IC}_{50, \text{app}}} \quad (12-13)$$

$$\text{PS} = \text{PS}_0 + (\text{PS}_I - \text{PS}_0) \times \frac{[S]}{[S] + K_{m, \text{app}}} \quad (12-14)$$

Differences in  $\text{IC}_{50, \text{app}}$  and  $K_{m, \text{app}}$  calculated by standard equations in current use vs. those suggested herein can be illustrated by substituting PS from Eq. (12-11) into Eq. (12-13) and solving for  $\text{IC}_{50, \text{app}}$  and by substituting PS from Eq. (12-12) into Eq. (12-14) and solving for  $K_{m, \text{app}}$ :

$$\text{IC}_{50, \text{app}} = \text{IC}_{50} \times \frac{\text{PS}_I}{\text{PS}_0} = \text{IC}_{50} \times \text{ER}_{\text{max}} \quad (12-15)$$

$$K_{m, \text{app}} = K_m \times \frac{\text{PS}_I}{\text{PS}_0} = K_m \times \text{ER}_{\text{max}} \quad (12-16)$$

As can be seen from Eqs. (12-15) and (12-16), current methods used for calculating  $K_{m, \text{app}}$  or  $\text{IC}_{50, \text{app}}$  will result in overestimation of these parameters by a factor of  $\text{ER}_{\text{max}}$  (Fig. 4).

This overestimation poses a number of potential problems. The  $\text{ER}_{\text{max}}$  for a given model system is dependent on both the efflux activity of the system and the test substrate. When  $\text{ER}_{\text{max}}$  is small, the relative error in  $K_{m, \text{app}}$  or  $\text{IC}_{50, \text{app}}$

calculated from current methods will be small. However, model systems with high efflux activity and substrates with large  $\text{ER}_{\text{max}}$  are precisely the model systems and substrates that are most sensitive for identifying efflux substrates and inhibitors. The  $\text{IC}_{50, \text{app}}$  of inhibitors should be properly ranked-ordered if testing is conducted with a common probe substrate and in a model system with a consistent efflux activity. However, when inhibitors are tested against dissimilar substrates and in different model systems expressing different efflux activity, then  $\text{IC}_{50, \text{app}}$  and rank ordering of  $\text{IC}_{50, \text{app}}$  may not correspond to the real  $\text{IC}_{50}$  or even the actual rank order. Lastly, the  $\text{IC}_{50, \text{app}}$  of the same inhibitor will differ between different substrates if the substrates have different  $\text{ER}_{\text{max}}$ . This behavior may confound results or be attributed incorrectly to inhibition at different binding sites on the efflux transporter for different substrates.

The situation in which  $K_{m, \text{app}}$  is affected by  $\text{ER}_{\text{max}}$  can be demonstrated by a recently reported study examining the flux of taurocholate through apical sodium-dependent bile acid transporter (hASBT). In this study with transfected MDCK monolayers, the  $K_{m, \text{app}}$  of taurocholate was shown to increase as a function of hASBT expression. This unexpected and novel observation was attributed to aqueous boundary layer effects (23). Alternatively, since transporter expression and  $\text{PS}_{\text{efflux}}$  are proportional, the observation is entirely consistent with the expected relationship between  $K_{m, \text{app}}$  and transporter expression [Eq. (12-16)]. If the  $K_m$  been calculated in a manner consistent with the kinetic model in Fig. 1 [Eq. 12-12], it is likely that that the "true"  $K_m$  would have been shown to be independent of hASBT expression, as expected.

### Inhibiting Active Efflux to Reverse MDR or Increase Drug Brain Penetration

Arbitrarily, reversal of multidrug resistance (MDR) can be defined as less than a twofold difference in intracellular drug concentrations between naïve cells and MDR cells. The change in PS necessary to reverse MDR then can be defined accordingly by:

$$\text{fold } \Delta \text{PS} \geq \frac{\text{ER}_{\text{max}}}{2} \quad (13-1)$$

From Eqs. (13-1) and (12-9), the degree of inhibition required to reverse MDR can be solved as:

$$\phi_i \geq \frac{\text{ER}_{\text{max}} - 2}{\text{ER}_{\text{max}} - 1} \quad (13-2)$$

The degree of efflux inhibition needed to reverse MDR therefore is dependent on  $\text{ER}_{\text{max}}$ . The higher the degree of MDR resistance, the higher the requisite degree of inhibition to reverse MDR. The inhibitor concentration necessary to reverse MDR can be determined by solving Eq. (13-2) for [I], assuming  $\phi_i = \frac{[I]}{[I] + K_i}$ :

$$[I] \geq (\text{ER}_{\text{max}} - 2)K_i \quad (13-3)$$

In Eqs. (13-2) or (13-3), all positive values  $\phi_i$  or [I] indicate the degree of inhibition or the inhibitor concentration necessary to inhibit efflux such that there is less than a twofold difference in drug resistance between MDR cells and naïve cell lines.

The degree of efflux inhibition necessary to reverse multidrug resistance is not simply a function of inhibitor  $K_i$  but also is dependent on  $ER_{max}$ . As cells become more resistant due to higher expression of the efflux transporter, the  $ER_{max}$  will increase, which will necessitate greater inhibition and consequently higher inhibitor concentrations to reverse MDR. Treatment with an efflux inhibitor will not reverse MDR in all cells equally, and will be less effective in cells possessing the highest degree of MDR. This, in turn, will result in tumors becoming more resistant because the most resistant cells will have a survival advantage. The relationships in Eqs. (13–2) and (13–3) are also applicable to reversing efflux at the blood–brain barrier in order to increase drug delivery of efflux substrates to the brain; substrates with larger values of  $ER_{max}$  will require a higher degree of efflux inhibition and higher inhibitor concentrations to overcome efflux.

A relevant case study to illustrate this point comes from a clinical study in which the specific P-gp inhibitor tariquidar was shown to completely inhibit P-gp in T lymphocytes [using the fluorescent dye DiOC<sub>2</sub> (3) as a probe], but was ineffective at inhibiting P-gp at the blood-brain barrier (using the opioid loperamide as a probe) (24). On first consideration, such observations may seem unexpected, and therefore lead to complex hypotheses to rectify apparently anomalous results. However, these observations are not, in fact, inconsistent. The  $ER_{max}$  of DiOC<sub>2</sub> (3) in T lymphocytes is ~4 (25), while the  $ER_{max}$  of loperamide at the blood-brain barrier has been estimated in preclinical experiments to be ~65 (26). Based on Eqs. (13–2) and (13–3) and the difference in  $ER_{max}$  between DiOC<sub>2</sub> (3) and loperamide, it is not surprising that complete inhibition of P-gp was observed in T lymphocytes but not in the blood-brain barrier.

## CONCLUSION

A set of equations, based on a simple three-compartment model, was derived to describe the theoretical relationships between  $PS_{efflux}$  and  $PS$ ,  $ER$ ,  $\phi_i$ ,  $IC_{50}$ , and  $K_m$ . The resulting relationships show that current mathematical treatment of efflux data is inconsistent with this model. In particular, these relationships mistakenly assume that  $PS_{efflux}$  is proportional to the attenuation or enhancement in  $PS$ , and that 50% inhibition of efflux activity will result in 50% of the maximum possible change in  $PS$ . The theoretical relationships derived herein indicate that such an assumption will lead to an overestimate of  $\phi_i$ ,  $K_m$  and  $IC_{50}$  in proportion to the  $ER_{max}$  of the experimental system. These relationships also show that  $PS_{efflux}$  is proportional to the passive permeability multiplied by  $ER-1$ , and that 50% inhibition of efflux activity will result in at most a twofold increase in  $PS$ . In addition, apical efflux has a minimum impact on the B-to-A flux ( $\leq$  twofold), and consequently B-to-A efflux studies are insensitive approaches for estimating efflux kinetic parameters. Finally, the three-compartment model and kinetic considerations indicate that a larger degree of efflux inhibition is necessary to reverse the effects of efflux when the efflux ratio is large. Viewing efflux activity in terms of efflux ratios rather than change in  $PS$  allows for better conceptual understanding and more accurate estimation of kinetic parameters; therefore, it is recommended that efflux

ratio be calculated and used when evaluating efflux activity and estimating the degree of efflux inhibition,  $IC_{50}$ , or  $K_m$ .

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